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Translation from: Referativnyy zhurnal, Khimiya, 1959, Nr 5, p 352 (USSR)

AUTHORS: Tsynkina, V.M., Gul'ko, N.V.

TITLE: Refractories From Strontium and Barium Compounds

PERIODICAL: Sb. nauchn. tr. Vses. n.-i. in-ta ogneuporov, 1958, Nr 2 (49), pp 297 - 318

ABSTRACT: The possibility was investigated of obtaining highly refractory articles based on Sr and Ba compounds. It was established that SrO can be used in the production of refractories (R) (burning at 1,750°C, grain size $< 60\mu$, porosity after burning 26 - 27%). The products are hydrated in air. It is recommended that admixtures of BeO and Al_2O_3 be added to the products of SrO to avoid this. R cannot be obtained from BaO by the usual method, since BaO is hydrated intensively in air, and Ba hydroxide, in admixture with BaO, melts at a temperature of $<$ 1,000°C when heated, which leads to fusion of the products. Zirconates of Sr and Ba are synthesized in the solid phase at a temperature of 1,000°C (tables of the properties of products made of Sr and

Card 1/ 2

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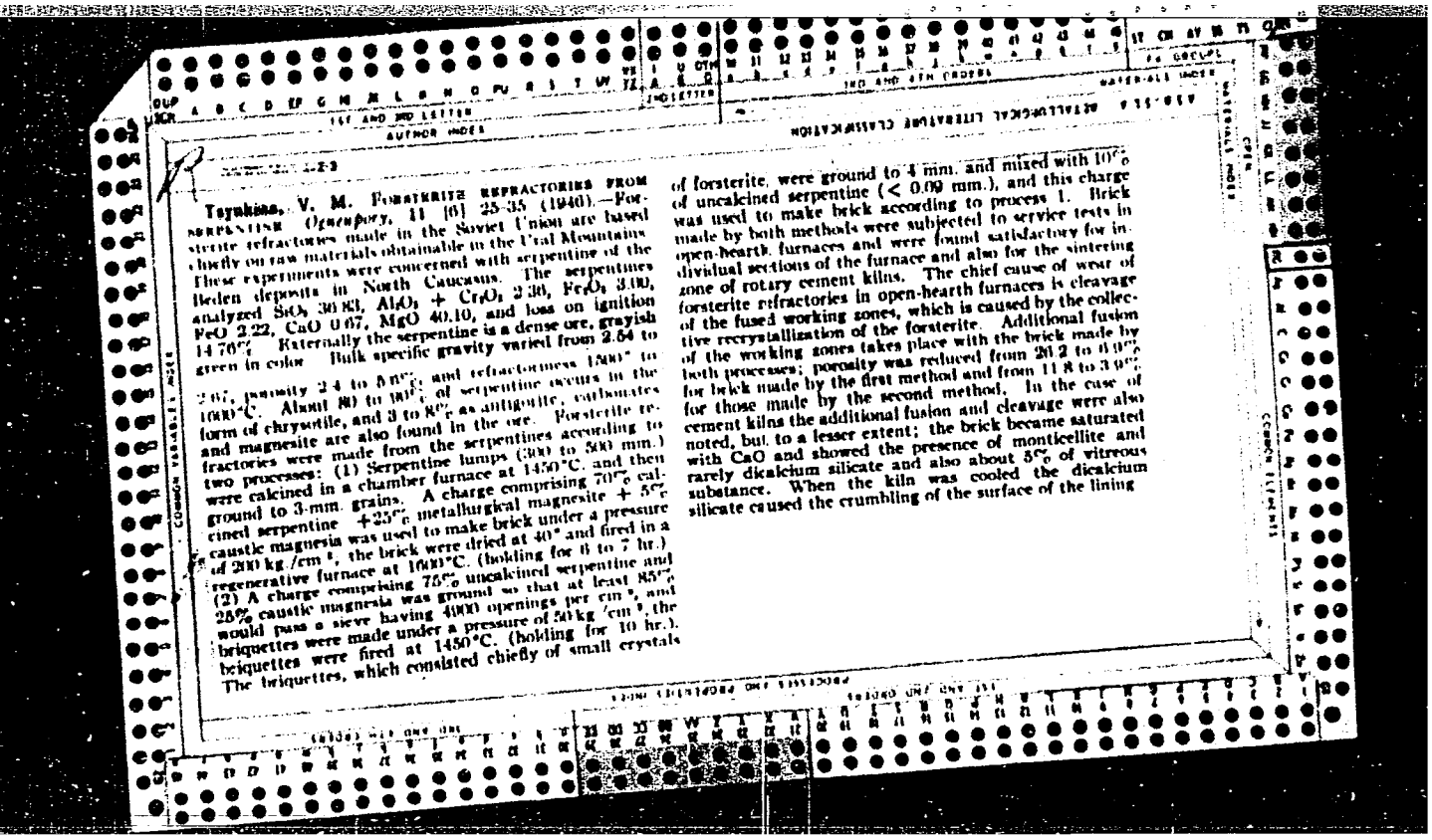
Refractories From Strontium and Barium Compounds

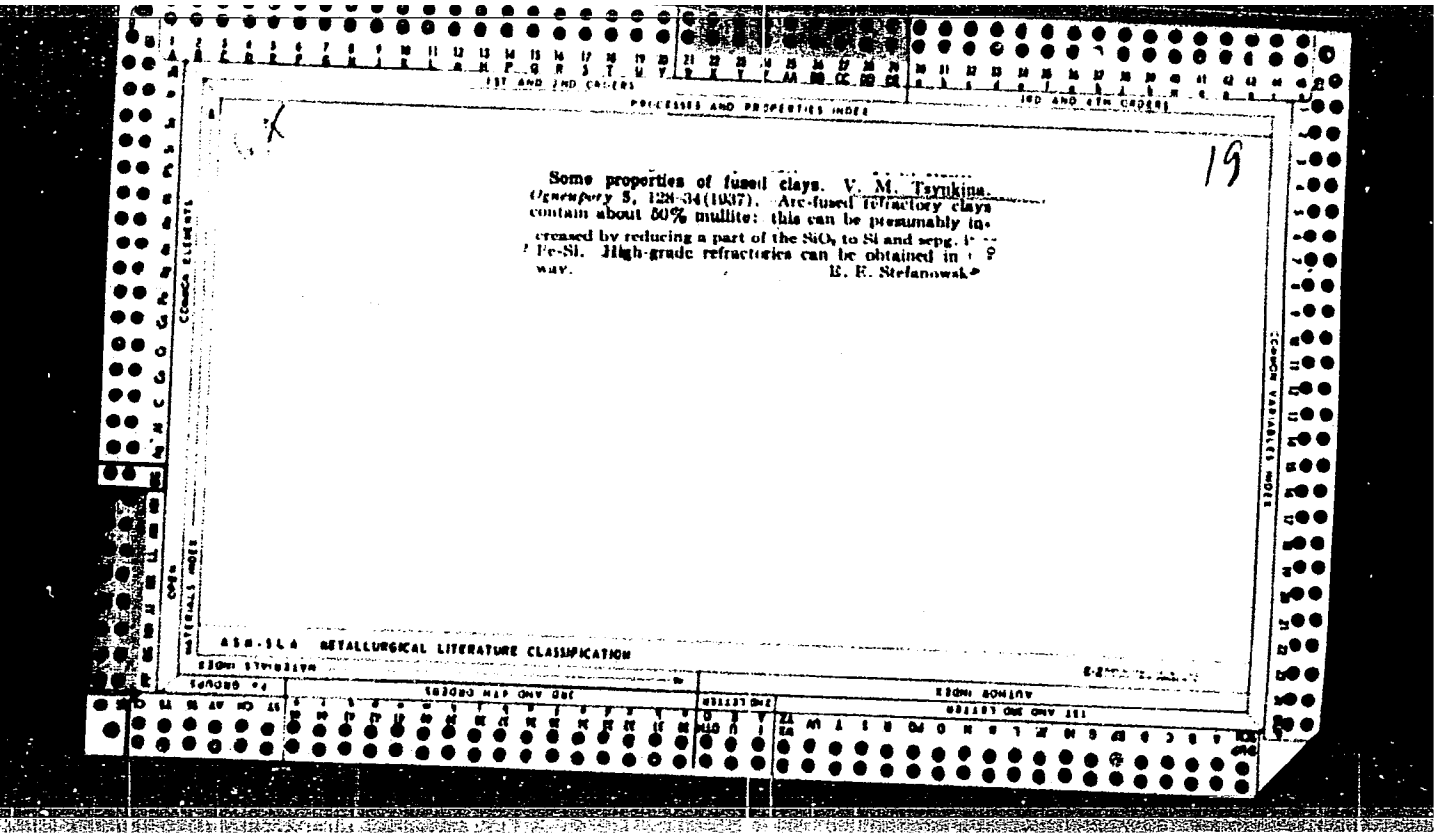
Ba zirconates are submitted). R made of Sr and Ba zirconates are highly refractory and are not hydrated during burning at 1,750°C. The orthosilicates of Sr and Ba were synthesized, the refractoriness was 1,750 and 1,910°C, respectively. R made of these have a high density and are not subject to hydration in air. The aluminates of Sr and Ba were synthesized; their properties were studied and R articles were produced from them. It is established that tristrontium and tribarium aluminates belong to the group of non-refractory compounds. Monoaluminates and hexaaluminates of Sr and Ba are not subject to hydration in air. The monoaluminate of Sr (porosity 1%) has a refractoriness of 1,800°C. R from zirconates, silicates and aluminates of Sr and Ba can be produced by briquetting with double burning of the briquet and intermediate crushing (size of the grain $< 60\mu$).

I. Mikhaylova

Card 2/2



Tsyukina, V. M. FORSTERITE REFRACTORIES FROM SERPENTINE. *Ogneupory*, 11 [6] 25-35 (1940).—Forsterite refractories made in the Soviet Union are based chiefly on raw materials obtainable in the Ural Mountains. These experiments were concerned with serpentine of the Bolden deposits in North Caucasus. The serpentines analyzed SiO_2 30.83, Al_2O_3 + Cr_2O_3 2.30, Fe_2O_3 3.10, FeO 2.22, CaO 0.67, MgO 40.10, and loss on ignition 14.76%. Externally the serpentine is a dense ore, grayish green in color. Bulk specific gravity varied from 2.54 to 2.67, porosity 2.4 to 8.8%, and refractoriness 1580° to 1600°C. About 80 to 90% of serpentine occurs in the form of chrysotile, and 3 to 8% as antigorite; carbonates and magnesite are also found in the ore. Forsterite refractories were made from the serpentines according to two processes: (1) Serpentine lumps (300 to 500 mm.) were calcined in a chamber furnace at 1450°C. and then ground to 3-mm. grains. A charge comprising 70% calcined serpentine +25% metallurgical magnesite + 5% caustic magnesia was used to make brick under a pressure of 200 kg /cm², the brick were dried at 40° and fired in a regenerative furnace at 1600°C. (holding for 6 to 7 hr.) (2) A charge comprising 75% uncalcined serpentine and 25% caustic magnesia was ground so that at least 85% would pass a sieve having 4900 openings per cm², and briquettes were made under a pressure of 50 kg /cm², the briquettes were fired at 1450°C. (holding for 10 hr.). The briquettes, which consisted chiefly of small crystals of forsterite, were ground to 4 mm. and mixed with 10% of uncalcined serpentine (< 0.09 mm.), and this charge was used to make brick according to process 1. Brick made by both methods were subjected to service tests in open-hearth furnaces and were found satisfactory for individual sections of the furnace and also for the sintering zone of rotary cement kilns. The chief cause of wear of forsterite refractories in open-hearth furnaces is cleavage of the fused working zones, which is caused by the collective recrystallization of the forsterite. Additional fusion of the working zones takes place with the brick made by both processes; porosity was reduced from 20.2 to 0.0% for brick made by the first method and from 11.8 to 3.0% for those made by the second method. In the case of cement kilns the additional fusion and cleavage were also noted, but to a lesser extent; the brick became saturated with CaO and showed the presence of monticellite and rarely dicalcium silicate and also about 5% of vitreous substance. When the kiln was cooled the dicalcium silicate caused the crumbling of the surface of the lining.



PROCESSES AND PROPERTIES INDEX

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Some properties of fused clays. V. M. Tsyrukina. *Ogneupory* 5, 128-34(1937). Arc-fused refractory clays contain about 80% mullite; this can be presumably increased by reducing a part of the SiO_2 to Si and segg. [illegible] Fe-Si. High-grade refractories can be obtained in [illegible] way. E. E. Stefanowska

ASM-SLA METALLURGICAL LITERATURE CLASSIFICATION

Thermostable magnesite refractories with a spinel mortar. A. S. BEREZHNOI AND V. M. TSVNKINA. *Sbornik Materialov po Voprosu Ogneuporoi Prom.*, 1939, No. 2, pp. 38–103; *Khim. Referat. Zhur.*, 4 [9] 110–11 (1941). —Results of experiments show the possibility of producing high-quality thermostable refractories from Satkin magnesite. A study of the formation of various spinels at high temperature, primarily through reactions in the solid phase, showed that alumina and chrome spinels are the most suitable. A technological procedure is recommended based on the study of the interdependence between the properties of fired magnesite and the methods of its production. A review of the literature and a description of technological works are included. See "Production. . . ." *Ceram. Abs.*, 18 [9] 245 (1939); "Spinel . . ." *ibid.*, 19 [3] 68 (1940).

M Ho.

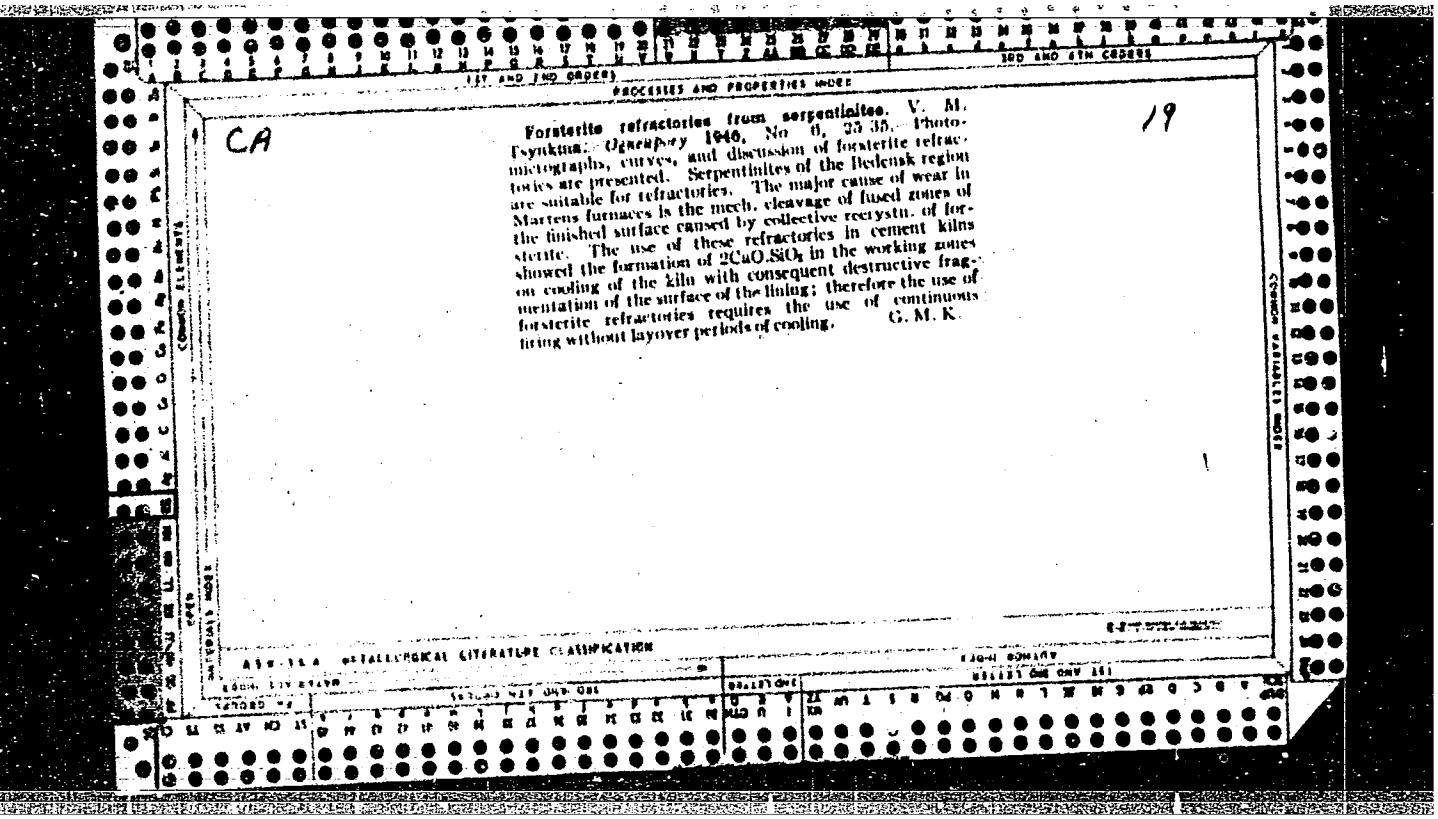
Bv. abs

B1-9 Glass; Ceramics; Refractories

Highly refractory oxides. V. M. Tsyrkina. (*Kislorod*, 1948, 9, Nos. 2—3, 56; *Brit. ceram. Abstr.*, 1949, 58A).—ThO_2 has a low thermal conductivity, but a high coeff. of thermal expansion; it is thus sensitive to spalling. It forms a carbide readily. Notes are given on the stabilisation of ZrO_2. Satisfactory results were obtained with ZrO_2 bricks in an open-hearth furnace. [illegible] in an unspecified position in an open-hearth furnace. [illegible] results were

R. B. CLARKE.

334. FORSTERITE REFRACTORIES FROM SERPENTINES – V. M. Teynkina (*Ogneupory*, 11, No. 6, 25, 1946). Forsterite refractories based on Russian serpentines were made up from calcined serpentine and magnesite, from sintered mixtures of the two, and from synthetic forsterite. Trials in the back wall of an open-hearth furnace and in the sintering zone of a rotary cement kiln proved that the forsterite refractories were equal to magnesite in performance in the open-hearth furnace where they were not exposed to silica drip from the roof, and were superior to the usual lining bricks in the cement kiln. Final failure in both furnaces was due to excessive shrinkage of the bricks near the working face. Absorption of lime and recrystallisation of the forsterite were observed up to 6 in. behind the working face, and it is suggested that recrystallisation was the primary cause of the shrinkage and consequent flaking. Addition of chromite is put forward as a possible cure for the shrinkage. The three types of forsterite product were not found to differ greatly in performance.



CA

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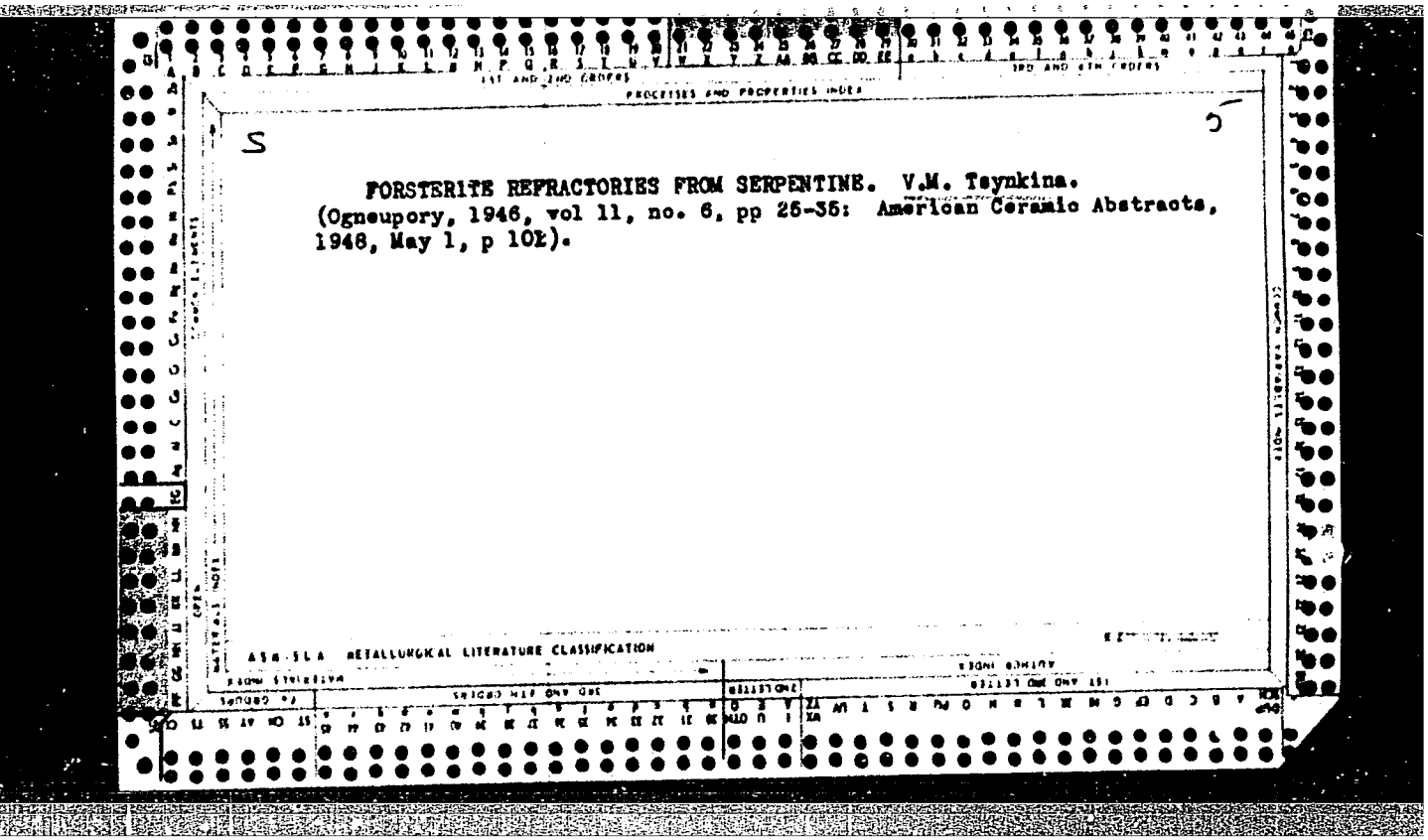
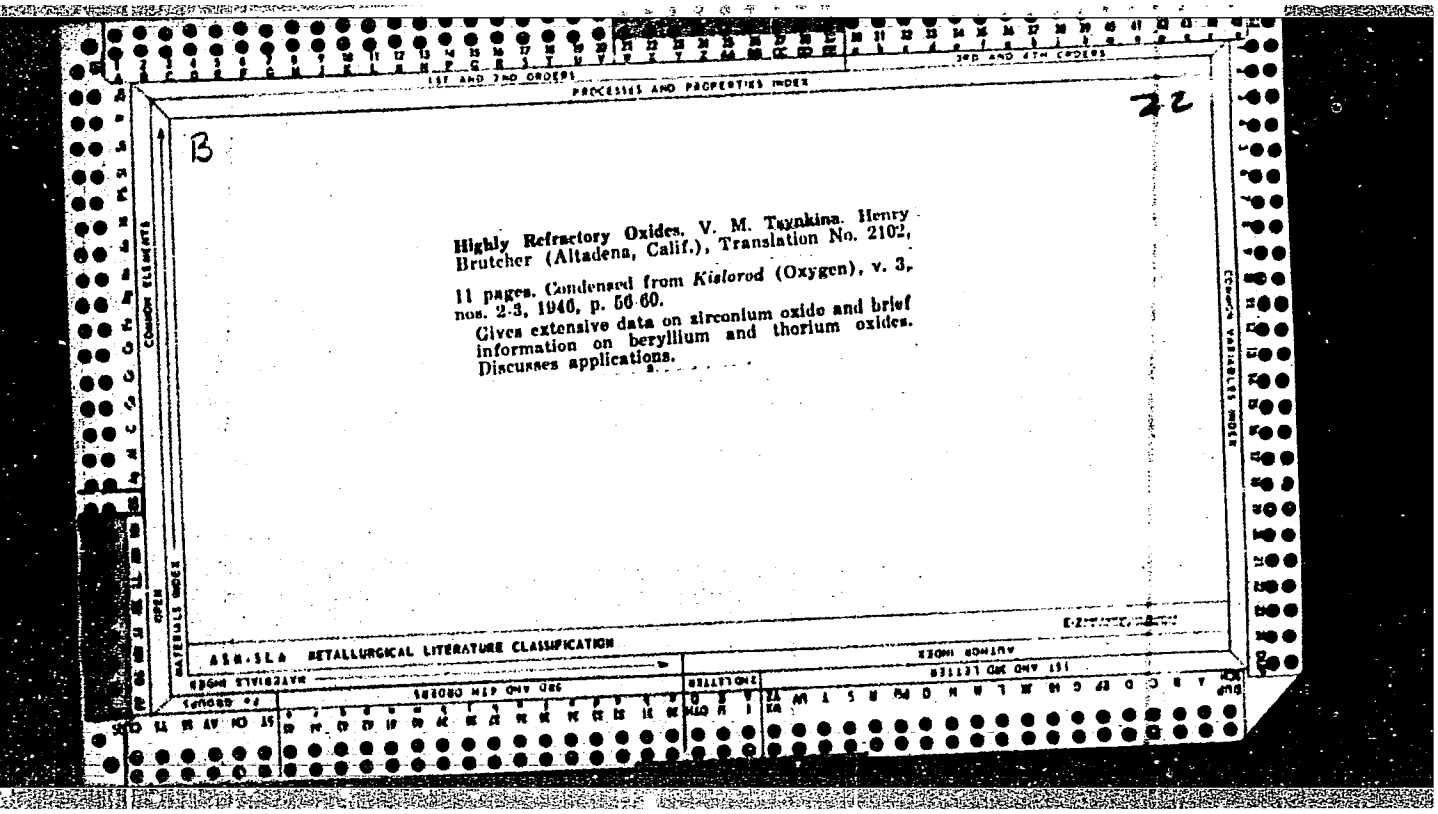
Forsterite refractories from serpentinites. V. M. Tsyuktsa. *Ogneupory* **1946**, No. 6, 33-35. Photomicrographs, curves, and discussion of forsterite refractories are presented. Serpentinites of the Bedenak region are suitable for refractories. The major cause of wear in Martens furnaces is the mech. cleavage of fused zones of the finished surface caused by collective recrystn. of forsterite. The use of these refractories in cement kilns showed the formation of $2CaO.SiO_2$ in the working zones on cooling of the kiln with consequent destructive fragmentation of the surface of the lining; therefore the use of forsterite refractories requires the use of continuous firing without layover periods of cooling. G. M. K.



FORSTERITE REFRACTORIES FROM SERPENTINE. V.M. Teynkina. (Ogneupory, 1946, vol 11, no. 6, pp 25-35: American Ceramic Abstracts, 1948, May 1, p 10Z).



B

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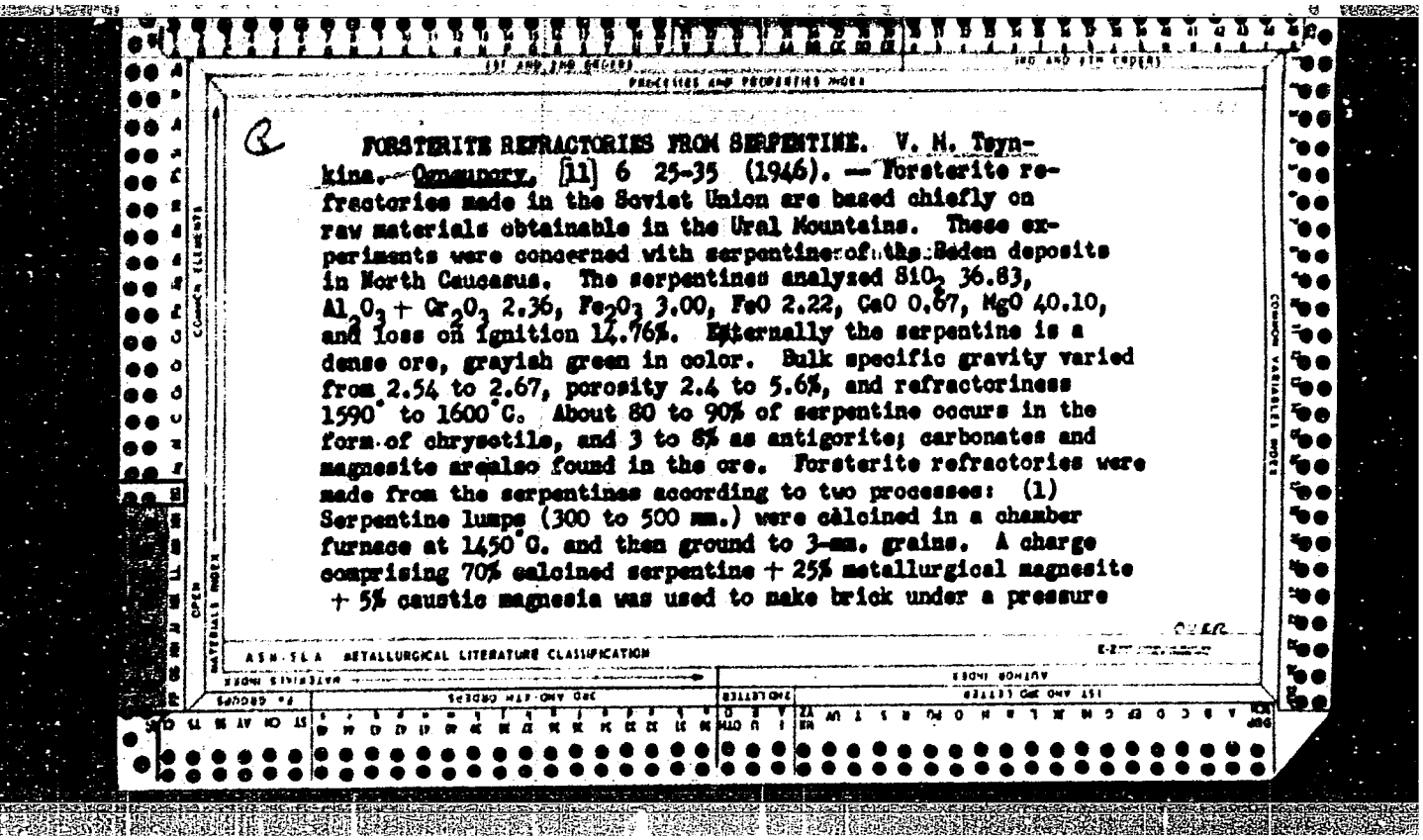
Highly Refractory Oxides. V. M. Tsynkina. Henry Brutcher (Altadena, Calif.), Translation No. 2102, 11 pages. Condensed from *Kislorod* (Oxygen), v. 3, nos. 2-3, 1940, p. 56-60.

Gives extensive data on zirconium oxide and brief information on beryllium and thorium oxides. Discusses applications.



Q

FORSTERITE REFRACTORIES FROM SERPENTINE. V. M. Teynkina. Ogneupory. [11] 6 25-35 (1946). — Forsterite refractories made in the Soviet Union are based chiefly on raw materials obtainable in the Ural Mountains. These experiments were concerned with serpentine of the Baden deposits in North Caucasus. The serpentines analyzed SiO_2 36.83, $Al_2O_3 + Cr_2O_3$ 2.36, Fe_2O_3 3.00, FeO 2.22, CaO 0.67, MgO 40.10, and loss on ignition 14.76%. Externally the serpentine is a dense ore, grayish green in color. Bulk specific gravity varied from 2.54 to 2.67, porosity 2.4 to 5.6%, and refractoriness 1590° to 1600° C. About 80 to 90% of serpentine occurs in the form of chrysotile, and 3 to 8% as antigorite; carbonates and magnesite are also found in the ore. Forsterite refractories were made from the serpentines according to two processes: (1) Serpentine lumps (300 to 500 mm.) were calcined in a chamber furnace at 1450° C. and then ground to 3-mm. grains. A charge comprising 70% calcined serpentine + 25% metallurgical magnesite + 5% caustic magnesia was used to make brick under a pressure

of 200 kg./cm.^{2}; the brick were dried at 40° and fired in a regenerative furnace at 1600°C. (holding for 6 to 7 hr.). (2) A charge comprising 75% uncalcined serpentine and 25% caustic magnesia was ground so that at least 85% would pass a sieve having 4900 openings per cm.^{2}, and briquettes were made under a pressure of 50 kg./cm.^{2}; the briquettes were fired at 1450°C. (holding for 10 hr.). The briquettes, which consisted chiefly of small crystals of forsterite, were ground to 4 mm. and mixed with 10% of uncalcined serpentine (< 0.09 mm.), and this charge was used to make brick according to process 1. Brick made by both methods were subjected to service tests in open-hearth furnaces is cleavage of the fused working zones which is caused by the collective recrystallisation of the forsterite. Additional fusion of the working zones takes place with the brick made by both processes; porosity was reduced from 26.2 to 6.9% for brick made by the first method and from 11.8 to 3.9% for those made by the second method. In the case of cement kilns the additional fusion and cleavage were also noted, but to a lesser extent; the brick became saturated with CaO and showed the presence of monticellite and rarely dicalcium silicate and also about 5% of vitreous substance. When the kiln was cooled the dicalcium silicate caused the crumbling of the surface of the lining.

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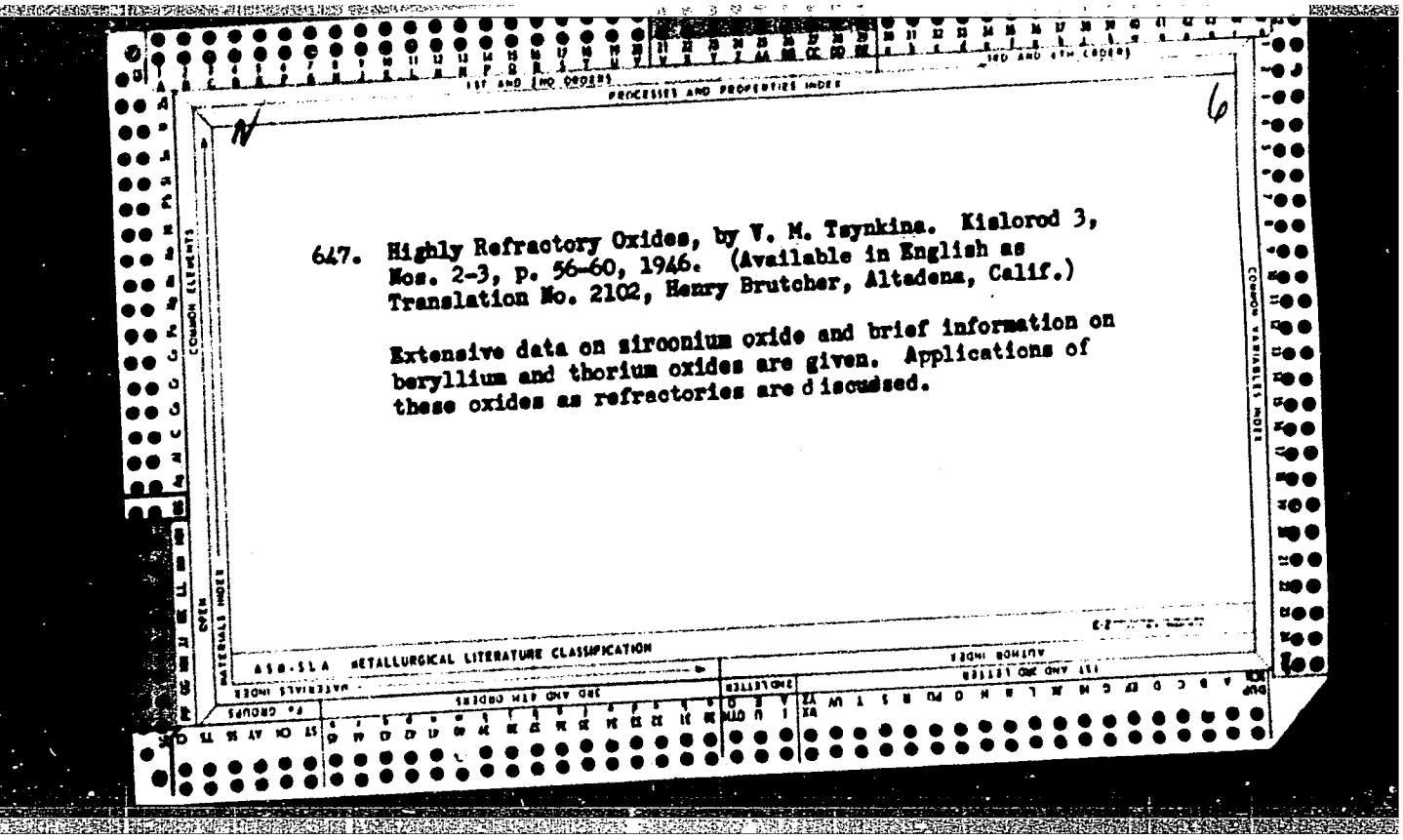


647. Highly Refractory Oxides, by V. M. Tsynkina. Kislorod 3, Nos. 2-3, p. 56-60, 1946. (Available in English as Translation No. 2102, Henry Brutcher, Altadena, Calif.)

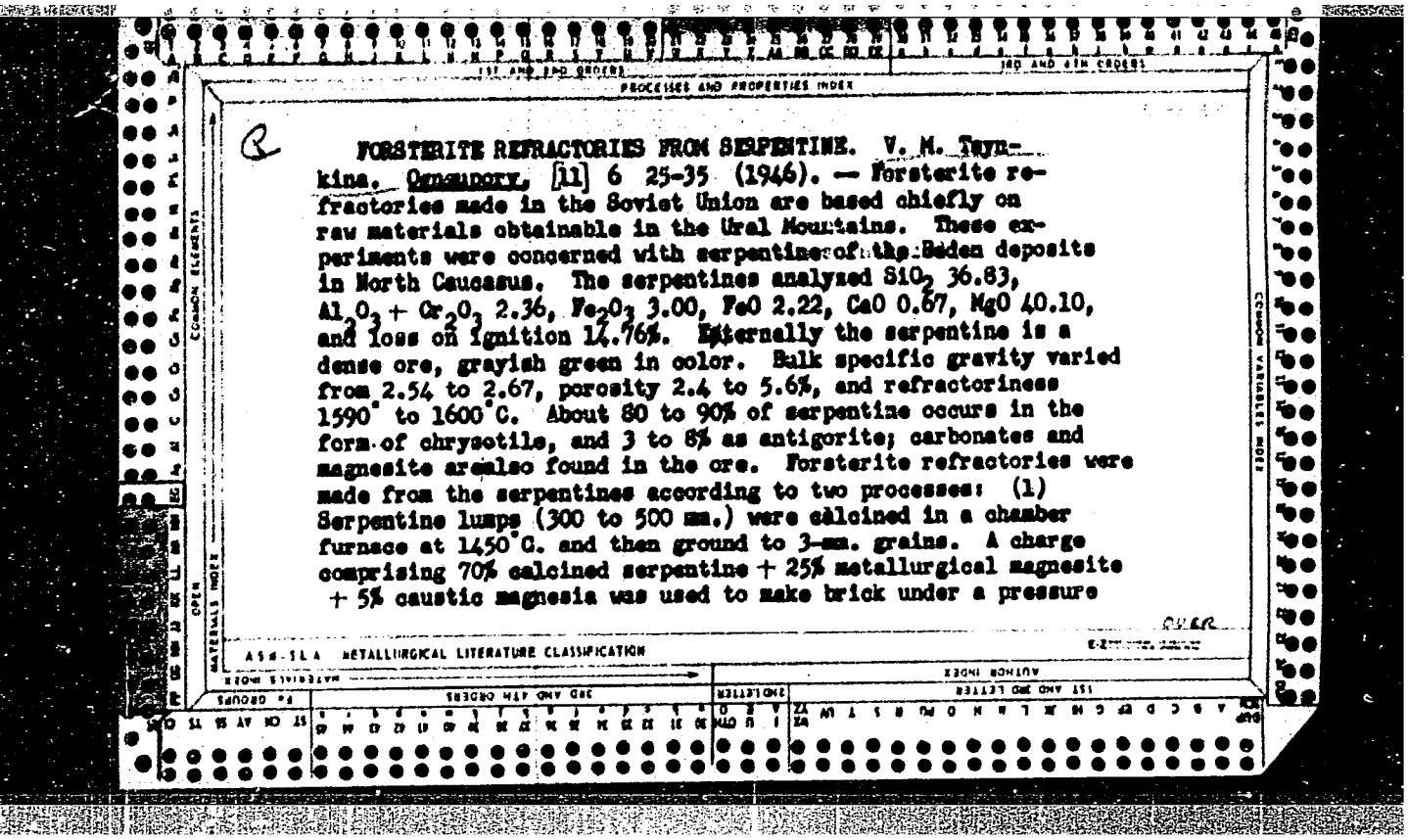
Extensive data on zirconium oxide and brief information on beryllium and thorium oxides are given. Applications of these oxides as refractories are discussed.

Br. Abs.

B1-4, Glass, Ceramics

Forsterite refractories from serpentines. V. M. Tsvetkina (*Ogneupory*, 1946, 11, No. 6, 23; *Brit. Ceram. Abs.*, 1947, 64A).—Refractories were made from calcined serpentine and magnesite, from sintered mixtures of the two, and from synthetic forsterite. Trials in the back wall of an open-hearth furnace and in the sintering zone of a rotary cement kiln showed forsterite refractories to be equal to magnesite in performance in the furnace where they were not exposed to SiO_2 drip from the roof, and better than the usual lining bricks for the kiln. Final failure in both cases was due to excessive shrinkage of the bricks near the working face. Absorption of CaO and recrystallisation of forsterite were observed up to 6 in. behind the working face; recrystallisation was probably the primary cause of shrinkage and subsequent flaking. Addition of chromite is suggested as a cure for shrinkage. The three types of forsterite product did not differ much in performance.

R. B. CLARKE.



R

FORSTERITE REFRACTORIES FROM SERPENTINE. V. M. Tsyn-kina. Ogneupory, [11] 6 25-35 (1946). — Forsterite refractories made in the Soviet Union are based chiefly on raw materials obtainable in the Ural Mountains. These experiments were concerned with serpentines of the Baden deposits in North Caucasus. The serpentines analyzed SiO_2 36.83, $Al_2O_3 + Cr_2O_3$ 2.36, Fe_2O_3 3.00, FeO 2.22, CaO 0.67, MgO 40.10, and loss on ignition 14.76%. Externally the serpentine is a dense ore, grayish green in color. Bulk specific gravity varied from 2.54 to 2.67, porosity 2.4 to 5.6%, and refractoriness 1590° to 1600°C. About 80 to 90% of serpentine occurs in the form of chrysotile, and 3 to 8% as antigorite; carbonates and magnesite are also found in the ore. Forsterite refractories were made from the serpentines according to two processes: (1) Serpentine lumps (300 to 500 mm.) were calcined in a chamber furnace at 1450°C. and then ground to 3-mm. grains. A charge comprising 70% calcined serpentine + 25% metallurgical magnesite + 5% caustic magnesia was used to make brick under a pressure

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(Firebrick—Testing)

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(Collective farms)

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[Economic effectiveness of sections of collective farms; a study] Ekonomicheskaia effektivnost' otraslei v kolkhozakh; opyt izucheniia. Moskva, Gos.izd-vo sel'khoz.lit-ry, 1957. 93 p. (MLRA 10:7)
(Agriculture--Costs)

1. TSYNKOV, M Yu.

2. USSR (600)

4. Collective Farms

7. "Correct combination of field crops and animal husbandry on collective farms." V. A. Kazanskiy. Reviewed by M. Yu. Tsynkov. Sov. zootekh. 7, no. 12, 1952.

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1. TSYNKOV, M. Yu

2. USSR (600)

4. Cattle

7. Stall system for keeping cattle, Sov. zootekh, 7, No. 11, 1952.

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1. TSYNKOV, M. Yu.

2. USSR (600)

4. Farm Management

7. "Correct combination of field crops and animal husbandry on collective farms." V. A. Kazanskiy. Reviewed by M. Yu. Tsynkov. Sov. zootekh. 7 no. 12, 1952.

9. Monthly List of Russian Accessions, Library of Congress, February 1953. Unclassified.

1. TSYTKOV, M. YU.

2. USSR (600)

4. Collective Farms

7. Correct ways of coordinating the branches of a consolidated consolidated collective farm Sov. zootekh./ No. 4, 1952

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TSYNKOV, M. YU

Dairing

Using feeding stuffs on progressive collective farms. Korm.baza., 2, no.12, 1951

Monthly List of Russian Accessions, Library of Congress, May 1952, UNCLASSIFIED.

1. M. YU. TSYNKOV
2. USSR (600)
4. Cattle - Feeding and Feeding Stuffs
7. Winter stall care of cattle. Dost. sel'khoz. no. 12. 1952.

9. Monthly List of Russian Accessions, Library of Congress, April 1953, Uncl.

TSYNKOVA, O. E. Cand Phys-Math Sci -- (diss) "Transient flow of gas in canals of finite length." Mos, 1959. 5 pp (Mos Order of Lenin and Order of Labor Red Banner State Univ im Lomonosov. Mechanical Math Faculty), 150 copies (KL, 52-59, 116)

TSYNKOV, Valeriy Mendelevich; ZUS'MAN, Il'ya Iosifovich; ZUBKOVA, M.S., red.

[Safety manual on the tensioning of reinforcement] Tekhnika bezopasnosti pri natiazhenii armatury. Moskva, Transport, 1964. 30 p. (MIRA 17:5)

AUTHOR: Tsynkova, O. E. (Moscow) SOV/179-59-3-3/45

TITLE: The Motion of a Gas Against a Variable Counter-Pressure in Channels of a Definite Length (Dvizheniya gaza v kanalakh konechnoy dliny pri peremennom protivodavlenii)

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Mekhanika i mashinostroyeniye, 1959, Nr 3, pp 15-24 (USSR)

ABSTRACT: A problem is described where the gas is flowing in channels having apertures in their walls (Fig 1). The system of equations describing the motion is given as Eq (1), where

p - pressure,
ρ - density,
u - velocity,
T - temperature,
S - enthropy,
i - full heat capacity per unit of mass of the gas,
t^o - time,
x - coordinate
Σ - cross-section of the channel
q - output of gas per unit of wall length,

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The Motion of a Gas Against a Variable Counter-Pressure in Channels of a Definite Length

u^* and i_o^* - mean mass,

p^* - mean pressure.

These equations can be shown as Eq (2) for the perfect gas and $\sum$ = const, with the variables p, ρ, u becoming a, ϑ, u, where a - sound velocity and $\vartheta = p/\rho^\gamma$ (γ - adiabatic index). Eq (2) can be presented in the linear form, Eqs (4), (5), for the conditions Eq (3). Its solution can be defined as Eq (6), where X = x and the functions F_1, F_2, F_3 are determined from Eq (11).

The limiting conditions can be derived for two cases: 1) the motion as in Fig 1. At the cross-section x = 0 there is a jump of density with the Mach number M_{10} in front and M_{20} behind. Since the jump is not stationary, the relation (12) can be derived (index 1 - disturbance added to the jump from the supersonic frequency of flow, index 2 - disturbance propagated behind the jump; D - velocity of jump in relation to the sound velocity a_{20} of the flow behind the jump,

The Motion of a Gas Against a Variable Counter-Pressure in Channels of a Definite Length

x^* - coordinate of the jump, μ, ν, $\varkappa$ etc - coefficients affected only by M_{10} and γ calculated from Eq (13)). It is assumed that the flow in front of the jump is not disturbed, i.e. $F_{11}(\zeta_1) = F_{31}(y_1) = 0$ in Eq (12). Then the limiting conditions for $x = x^*$ will take the form of Eq (14) which, in the linear form, can be written as Eq (15). By taking u and a in Eq(15) from Eqs (8) and (9), the formulae (16) and (17) are derived for the initial conditions (18). The solution of Eq (16) is given as Eq (19). The coefficients ν_0 and ζ_0 in Eq (19) can be called double coefficients of reflection. Fig 2 illustrates the relations of ν_0 and ζ_0 to M_{10} for $\gamma = 1.4$.

2) The velocity of flow is below that of sound, the linear equation of which is defined as Eq (21). Since the pressures of the flow in this case are equal, then for $p = 0$ and $x = 1$ the basic equation can be expressed as Eq (22) and its solution as Eqs (23), (25). If the

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resonance is considered (Eqs 27 and 29), then the solution will take the form of Eq (3). The amplitudes of variations of pressure, enthropy and the jump respectively are defined by Eq (31). These are illustrated in Fig 3.
The influence of external effects on the jump of density can be defined as Eq (32) which describes the velocity D (Eq 17). An example is given which is divided into two parts: first the general formulae are presented in the order of calculation (Eqs 33, 34 and 35) and next the results obtained from numerical data (foot of p 24) are presented.
There are 3 figures and 3 references, 1 of which is Soviet and 2 English.

SUBMITTED: December 25, 1958

RAUSHENBAKH, Boris Viktorovich; TSYNKOVA, O.E., red.; MURASHOVA, N.Ya., tekhn. red.

[Vibration combustion] Vibratsionnoe gorenie. Moskva, Gos. izd-vo fiziko-matem. lit-ry, 1961. 500 p. (MIRA 14:8)
(Combustion, Theory of) (Vibration)

67587
SOV/179-59-5-5/41

10.3000
AUTHOR: Tsynkova, O.E. (Moscow)

TITLE: On Self-Excited Oscillations in Supersonic Diffusers

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Mekhanika i mashinostroyeniye, 1959, Nr 5, pp 19-26 (USSR)

ABSTRACT: It is stated that in most previous investigations of supersonic diffuser stability, the low frequency oscillations (so-called pumping) were examined by formulating qualitative assumptions, partly confirmed by experimental data. Analysis is usually applied to cycles of fully established oscillations and is carried out on the assumption that the causes of the phenomenon are unknown. Thus, Dailey Charles L. ("Supersonic Diffuser Instability", - Ref 1), on the basis of experimental observations, assumes a certain sequence in the pumping process. An analysis of the process of filling the diffuser chamber is formulated in quasi-stationary terms, without consideration of the propagation of the waves in the internal flow passages. The differential equation reduces to an ordinary first order equation without periodic solutions. An additional specification of the maximum and

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On Self-Excited Oscillations in Supersonic Diffusers

minimum pressures in the diffuser chamber produces semi-empirically the duration of the pumping cycle. Later work is mentioned wherein the criteria of stability are mathematically formulated. It is concluded that established pumping with a correct periodicity is possible only when the critical cross-section of the diffuser exit is below the value corresponding to the conditions of maximum pressure build-up. Although the conclusion is verified by many experiments, the method of small perturbations used does not easily fit the pumping phenomenon. Oswatisch and Teipel (Ref 3) study the motion in which the beginning and the cyclic sequence of pumping is basically associated with the propagation of waves in the internal diffuser channel and the conditions at its end. The analysis of the pumping case is covered mathematically in the same manner as motion with decaying oscillations. However, the formulation of a general criterion to divide these stable and unstable conditions was not possible because the solution was obtained numerically. The present work solves the problems of self-excited oscillations by the method of linear travelling waves. For a cylindrical diffuser, the general solution

On Self-Excited Oscillations in Supersonic Diffusers

of linearised equations for the one-dimensional flow of an ideal gas with plane waves is recalled, expressing the deviations of velocity, sound velocity and entropy in terms of certain combinations of arbitrary functions which have to be fitted to the initial and end conditions. The stability critera are finally obtained directly from the solutions. An example is quoted wherein, with a diffuser channel of 1 m length and a speed of sound of the undisturbed flow in the channel amounting to 400 mps, pumping frequencies of 31, 28 and 25 cps were found. The throttling of the critical cross-section at the diffuser channel outlet leads to a condition of decaying oscillations or a condition of pumping according to the value of the sum of the reflexion coefficients at the open entry into the channel for the pressure and entropy waves, respectively. This leads to the separation of stable and unstable operating conditions which are characterized by the values of the tangent of the diffuser characteristic curve slope. The Pitot type diffuser (without central body) normally works under stable conditions. Pumping conditions are obtained in diffusers with a central body.

On Self-Excited Oscillations in Supersonic Diffusers

Apparently, this is explained by the presence of viscosity and cannot be explained within the framework of ideal gas theory. There are 2 figures and 4 references, 2 of which are Soviet, 1 English and 1 German.

SUBMITTED: May 9, 1959

Card 4/4

TSYHMAN, A.Yu.

Solving diagnostic problems in course on internal medicine. Fel'd. i akush. 21 no.2:53 F '56. (MLRA 9:5)

1. Bryanskoye meditsinskoye uchilishche.
(MEDICINE--STUDY AND TEACHING)

SOV/68-58-12-8/25

AUTHOR: Tsynovnikov, A.S., Shemeryankin, B.V., Shvarts, S.A. and Bogoyavlenskiy, K.A.

TITLE: The Determination of Size Analysis of Coke on Screens with Square and Round Mesh (Opredeleniye sitovogo sostava koksa na sitakh s kvadratnymi i kruglymi otverstiyami)

PERIODICAL: Koks i Khimiya, 1958, Nr 12, pp 25-28 (USSR)

ABSTRACT: The relationship between the size analysis of coke on screens with square and round mesh, namely the ratio of D : S (diameter of square mesh to diameter of round mesh) for cokes of various origin was investigated. The experimental results are shown in figs 1, 2, and Tables 1, 2. Coefficients (K) for recalculating size distribution from screens with round mesh to screens

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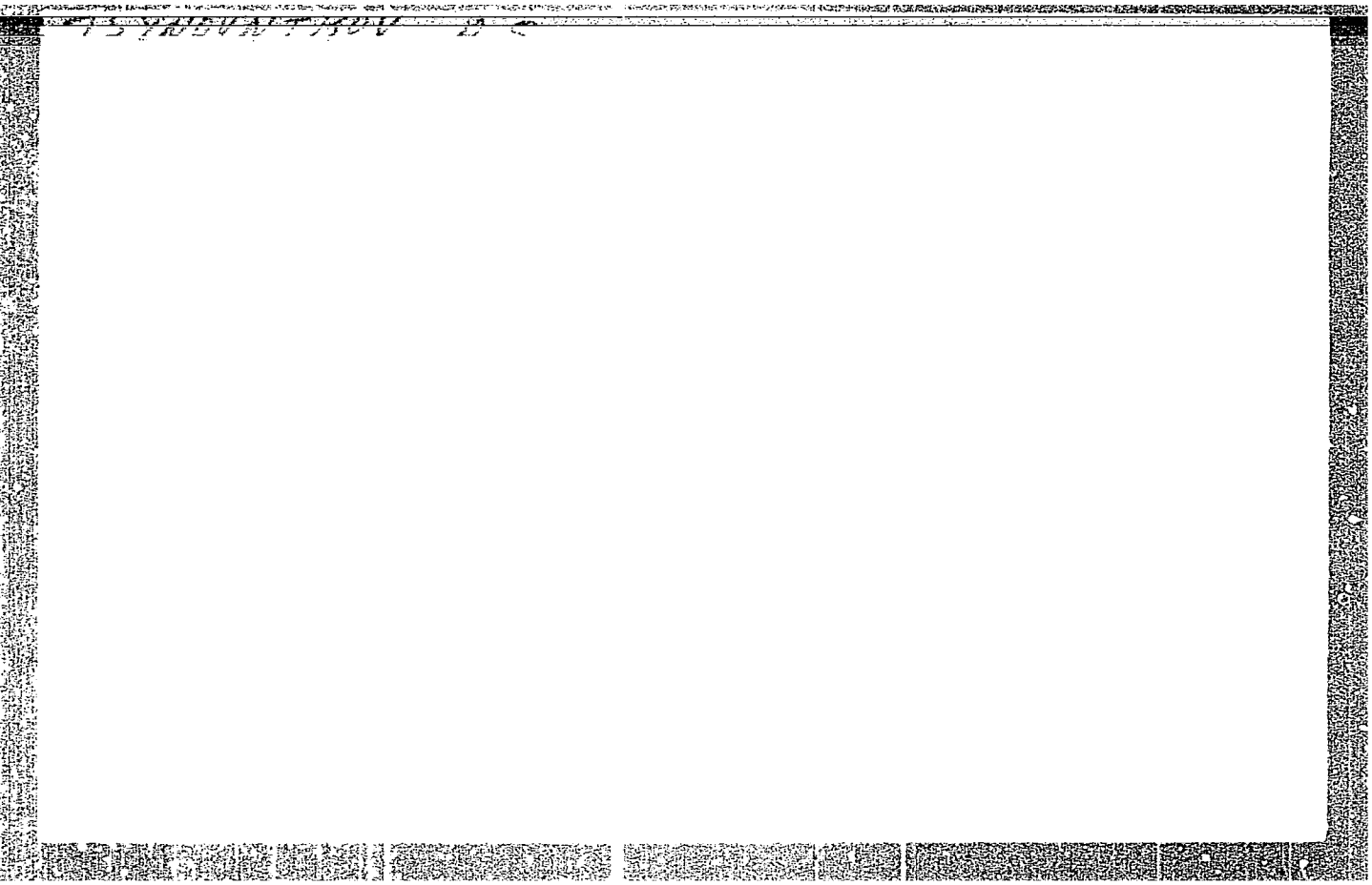
The Determination of Size Analysis of Coke on Screens with Square and Round Mesh

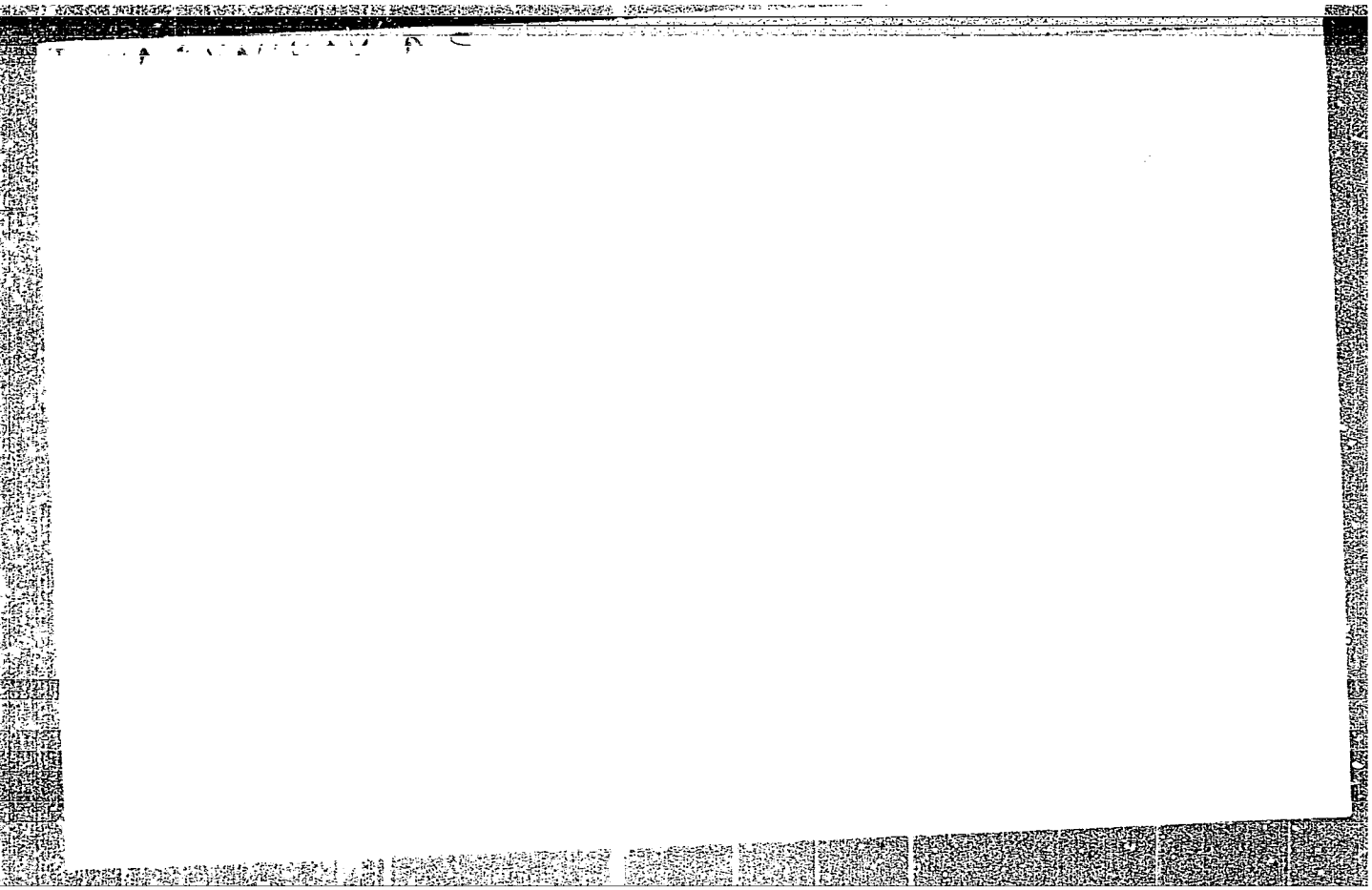
with square mesh for various types of coke are given in Table 3 and mesh sizes for round and square mesh screens for various size fractions in Table 4.

There are 4 tables and 2 figures.

ASSOCIATIONS: VUKhIN and UKhIN



APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001757320003-3"



APPROVED FOR RELEASE: 08/31/2001 CIA-RDP86-00513R001757320003-3"

TSYNOVNIKOV, A.S.; SHEMERYANKIN, B.V.; LIKHOGUB, Ye.P.; MUSTAFIN, F.A.; BERKUTOVA, G.I.

Increasing the charges of coke ovens during leveling. Koks i khim. no.2:19-22 '60. (MIRA 13:5)

1. Vostochnyy uglekhimicheskiy institut (for TSynovnikov, Shemeryankin). 2. Teplotekhstantsiya (for Likhogub). 3. Nizhne-Tagil'skiy metallurgicheskiy kombinat (for Mustafin, Berkutova). (Nizhniy Tagil--Coal--Carbonization)

SHEMERYANKIN, B.V.; TSYNOVNIKOV, A.S.; RYTCHENKO, A.I.

Bulk weight of coke. Koks i khim. no.8:30-33 '61. (MIRA 15:1)

1. Chelyabinskiy metallurgicheskiy zavod (for Shemeryankin).
2. Vostochnyy uglekhimicheskiy institut (for TSynovnikov).
3. Nizhne-Tagil'skiy metallurgicheskiy kombinat (for Rytchenko).
(Coke)

TSYNOVNIKOV, A.S.; MUSTAFIN, F.A.; GUSEV, A.P.

Preparation of coals and blended coal charges for coking. Koks i khim. no8:10-12 '56. (MIRA 10:1)

1. Vostochnyy uglekhimicheskiy institut (for TSynovnikov).2.Nizhne-Tagil'skiy koksokhimicheskiy zavod.
(Coal preparation)

TSYNOVNIKOV, A.S.; MUSTAFIN, F.A.

Utilizing coals with low caking power. Koks.i khim.no.5:6-9 '56.
(Coal) (Coke) (MLRA 9:10)

SPERANSKAYA, G.V.; TSYNOVNIKOV, A.S.; STROMBERG, B.I.

Experimental coking of coals enriched by centrifugal separation.
Koks i khim.no.4:8-11 '56. (MIRA 9:9)

1.Institut goryuchikh iskopayemykh Akademii nauk SSSR (for Speranskaya).2.Vostochnyy uglekhimicheskiy institut (for TSynovnikov).3. Ukrainskiy uglekhimicheskiy institut (for Shtremberg).
(Coal--Carbonization)

GRYAZNOV, N.S.; SHEMERYANKIN, B.V.; TSYNOVNIKOV, A.S.

Classification of coke according to types and sizes. Koks i khim. no.10:22-26 '60. (MIRA 13:10)

1. Vostochnyy uglekhimicheskiy institut.
(Coke)

TSYP, V. N.

TSYP, V. N.; CHERNAYA, L. A.; ZAKHARINA, D. I.

"Serotherapy of Experimental Gas Gangrene"

Annaly Mechnikovskogo Institut, Vol. 3, No. 1, 1936, pp 91-94
(Annals ((or Records)) of the Mechnikov Institute)
in
Report on the Research Work of the All-Union Institute of Experimental Medicine imeni A. M. Gor'kiy for 1933-1937, "Medgiz", Moscow-Leningrad, 1939 (book)—p 86

ACC NR: AP7006802 (A) SOURCE CODE: UR/0418/66/000/006/0084/0086

AUTHOR: Korenevskiy, Ye. Ya. (Engineer); Tsypak, V. I. (Engineer); Semenov, R. A. (Engineer)

ORG: None

TITLE: Effect of annealing and vibrotumbling on the durability of parts made from OT4-1 titanium alloy after surface grinding

SOURCE: Tekhnologiya i organizatsiya proizvodstva, no. 6, 1966, 84-86

TOPIC TAGS: titanium alloy, grinding, durability, annealing, surface finishing

ABSTRACT: Flat specimens of OT4-1 sheet titanium alloy 7 mm thick were studied for the effect of annealing and vibrotumbling on surface quality and durability after surface grinding. The grinding operation was done on a 372B unit with a K340M2B wheel at a speed of 25 mm/sec to a depth of 0.05 mm with a longitudinal feed of 7 m/min removing 0.3 mm from each side. An emulsion was used as coolant. After grinding, the flat surfaces of the specimen showed a class 6-7 finish, a microhardness of 250-270 kg/mm^2 and a cold-hardened layer 0.02-0.025 mm deep. Four sets of specimens were prepared: 20 specimens were left as they were after grinding; 15 specimens were annealed; 15 were subjected to vibrotumbling; 15 were subjected to vibrotumbling with subsequent annealing. The annealing was done at 540°C for 0.5 hour followed by cool-

Card 1/2 UDC: 669.295.620.178.3

ACC NR: AP7006802

ing in air. The vibrotumbling was done in GZh-1 anticorrosion fluid using steel balls 2 mm in diameter with a vibration speed of 0.96 m/sec at a vibration overload factor of 10.1 for 1.5 hours. It was found that annealing improves surface finish by about one class. Vibrotumbling also produced the same improvement in surface finish. Annealing reduces the microhardness of the surface both after grinding and after vibrotumbling. Vibrotumbling increases microhardness by 60 kg/mm^2. Vibrotumbling also improves the regularity of microhardness as compared with the initial specimens. It was also found that surface grinding results in a considerable reduction in the strength properties of OT4-1 titanium alloy. The fatigue limit of the initial material was reduced from 34-40 to 21 kg/mm^2 by grinding. The fatigue limit was increased by 31.9% in specimens subjected to annealing after grinding. Vibrotumbling raises the fatigue limit by 76.6% as compared with the initial specimens after grinding. Annealing after vibrotumbling removes the strength produced by this operation. Orig. art. has: 1 figure, 1 table.

SUB CODE: 13, 11/ SUBM DATE: None

Card 2/2

USSRDiseases of Farm Animals - Diseases Caused by Viruses and Rickettsiae. R-3

Abs Jour : Ref Zhur - Biol., No 14, 1958, 64654

Author : Tsyganov, D.M.
Inst : -
Title : Experience in the Control of Foot-and-Mouth Disease in Northern Reindeer.

Orig Pub : Veterinariya, 1957, No 12, 65-70

Abstract : The basic measure in combatting foot-and-mouth disease was that of a rigid quarantine of the suspected herds. The use of the VIEV vaccine on 46 thous. reindeer did not produce positive results. The peculiarities of the clinical and pathologicoanatomic picture in reindeer are described.

Card 1/1

USSR / Farm Animals. Reindeer. C-3

Abs Jour: Ref Zhur-Biol., No 23, 1958, 105739.

Author : Tsypanov, D. M.
Inst : Scientific Research Institute of Agriculture of the Extreme North.
Title : Organization of Communication with Distant Reindeer Breeding Brigades in Komi ASSR.

Orig Pub: Byul. nauchno-tekhn. inform. n.-i. in-t s.-kh. Krayn.

Abstract: No abstract.

Card 1/1

TSYPANOV, D.M., zasluzhennyy veterinarnyy vrach, Komi ASSR.

Eradicating foot-and-mouth disease among reindeer. Veterinariia 34 no.12:65-70 D '57. (MIRA 11:1)
(Reindeer--Diseases and pests)
(Foot-and mouth disease)

ROZHKOV, V.M.; TSYPER, V.A.; KRIVONOS, G.A.; CHERNOSHTAN, V.K.; SAPRYKIN, A.A.

Mastering the production of drill pipes with inner tips made of the B95 alloy. TSvet. met. 36 no.9:79-84 S '63. (MIRA 16:10)

ROZHKOV, V.M.; SHOFMAN, L.A.; ROZANOV, B.V.; KUZ'KO, Yu.P.; PONGIL'SKIY, N.F.; LIVANOV, V.A.; LUCHIN, V.V.; KUZNETSOV, K.I.; TSYPER, V.A.; CHERNOSHTAN, V.K.

Points for pipe presses. Biul.TSIICHM no.9:52 (MIRA 15:4)
(Pipe mills--Equipment and supplies)

L 13284-66 EWT(d)/EWT(m)/EWP(w)/EWP(c)/EWA(d)/EWP(v)/T/EWP(t)/EWP(k) EWP(h)/
EWP(z)/EWP(b)/EWP(l)/EWA(c)/ETC(m) IJP(c) MJW/JD/HW

ACC NR: AP6001105 (N) SOURCE CODE: UR/0136/65/000/012/0074/0076

AUTHOR: Molodchinin, Ye. V.; Tsyper, V. A.; Markin, M. G.

ORG: none

TITLE: The equipment and technological lubrication for the hot rolling of tubes of AMg6 aluminum-magnesium alloy

SOURCE: Tsvetnyye metally, no. 12, 1965, 74-76

TOPIC TAGS: aluminum base alloy, magnesium alloy, hot rolling, metal tube, lubricant / AMg6 Al-Mg alloy

ABSTRACT: Since the alloy AMg6 displays highest plastic properties in the temperature range 120-220°C, the rolling of tubes from this alloy is best performed on maintaining these temperatures over the area of deformation. In this connection the authors describe a method of stabilizing rolling technology by preheating the skelp to 100-150°C in an induction heater mounted directly on the KhPT type tube mill. The low-frequency induction-heating installation, operating on industrial-frequency current, consists of an inductor, a 300-kva stepdown transformer, a capacitor battery, a start-up panel, and busbars. The inductor itself (Fig. 1) represents a solenoid coil wound in two layers of rectangular copper tube 14x14 directly on circular stainless-steel liner 1. Insulation 2 of the 23 turns of the coil is of herringbone tape impregnated

Card 1/3 UDC: 669.715:621.771.2

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ACC NR: AP6001105

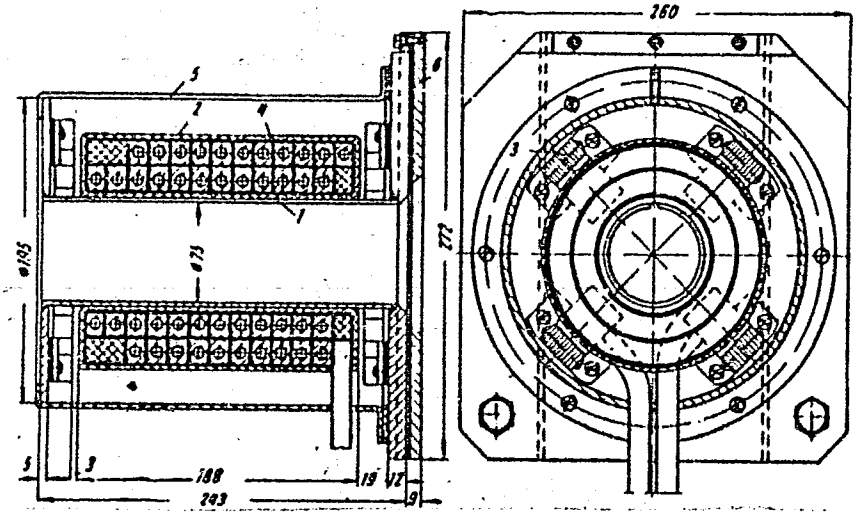


Fig. 1. Inductor for hot rolling of tubes in KhPT-75 tube mill

Card 2/3

L 13284-66

ACC NR: AP6001105

with bakelite varnish. To reduce magnetic leakage, four magnetic circuits are installed over the outside diameter of the inductor. The magnetic circuits and inductor winding 4 are insulated against lubricant contamination by housing 5 made of stainless sheet steel. The inductor is affixed to the bed of the rolling mill by means of plate 6. During rolling the friction of skelp at joints leads to the continual formation of metal chips which, unless promptly washed away by the lubricant, may enter the zone of deformation and adhere to the tools, thus causing imprints on the tubes. In this particular case the lubricant must be preheated to 60-80°C before applying it to the deformation zone. The authors tested a large number of the lubricants most suitable for operation in the temperature range 100-200°C. Unfortunately, so far not one has completely met the requirements, since at these temperatures heavy cylinder oils decompose and smoke and, moreover, are difficult to remove from the inside and outside tube surfaces. As for the spindle oil used for the cold rolling of tubes in tube mills, if applied in cold state it causes the cooling of the preheated skelp and hence the cracking of the tubes. The industrial introduction of the warm rolling of tubes of high-strength Al-Mg alloys has resulted in increasing by 30-40% the productivity of KhPT tube mills as well as in increasing by 5-7% the proportion of defect-free tubes. Orig. art. has: 2 figures.

SUB CODE: 11, 13/ SUBM DATE: none/ ORIG REF: 000/ OTH REF: 000

Card 3/3

VENDT, V. P., TSYPEROVYCH, A. A.

Tyrosine

Spectrographic investigation of changes in the reactivity of tyrosine groups in seous and ovular proteins during denaturation. Ukr. biokhim. zhur. 22, No. 1, 1950.

9. Monthly List of Russian Accessions, Library of Congress, October 1952 1653, Uncl.

TSYPEROVICH, A. S.

Tsyperovich, A. S. "On the mechanism of the denaturation of proteins, 3: The intermittent character of the thermal denaturation of serous and egg albumins", Ukr. biokhim. zhurnal, 1949, No. 1, p. 44-55, (In Ukrainian, resume in Russian), - Bibliog: 15 items.

SO: U-4630, 16 Sept. 53, (Letopis 'Zhurnal 'nykh Statey, No. 23, 1949).

TSYPKIN, Ya.Z.

Criterion of the absolute stability of pulse automatic systems with monotone characteristics of the nonlinear element. Dokl. AN SSSR 155 no. 5:1029-1032 Ap '64. (MIRA 17:5)

1. Institut avtomatiki i telemekhaniki AN SSSR. Predstavleno akademikom V.S.Kulebakinym.

Hydration and electric symmetry of molecules of denatured and natural egg albumin. O. D. Kurilenko and A. S. Tayperovich. *Doklady Akad. Nauk S.S.S.R.* 66, 349-52 (1949). The dielec. const. of egg albumin denatured with urea at 20° differs from that of native albumin especially at wavelengths of 35-50 m., being some 10% lower, while in 22-30 m. region it is 3-5% higher. Change of optical activity with increased extent of denaturation is linear. The increased dielec. const. at shorter wavelengths is probably assocd. with liberation of bound water, a conclusion apparently supported by the simultaneous change of slope of the optical activity and extent of denaturation curves. The relaxation period is essentially identical for the natural and the denatured states and the mol. wt. (36,000) is unchanged. The difference in the changes of dielec. const. cannot be correlated at this time with the progressive and smooth variation of optical activity.

G. M. Kosolapoff

TSYNOVNIKOV, A.S.; FILIPPOVA, A.A.

Selection of samples and the indices of coke properties.
Standartizatsiia 28 no.3:31-36 Mr'64. (MIRA 17:5)

VENDT, V. P., TSYPEROVICH, A. S.

Tyrosine.

Spectrographic investigation of changes in the reactivity of tyrosine groups in serous and ovular proteins during denaturation. Ukr.biokhim.zhur. 22 no. 1, 1950.

9. Monthly List of Russian Accessions, Library of Congress, October 1953, Uncl.

1. TSYPEROVYCH, A. S.

2. USSR (600)

4. Proteins

7. Mechanism of the denaturation of proteins. Part 5. Quasichemical equilibria in the denaturation of globular protein by urea, Ukr. biokhim. zhur., 24, no. 1, 1952.

9. Monthly List of Russian Accessions, Library of Congress, April 1953, Uncl.

TSYPEROVICH, A. S.

USSR/Chemistry - Proteins 11 Mar 52

"Completeness of Transformation of the Protein Molecule During Denaturation," V. A. Belitser, A. S. Tsyperovich, Inst of Biochem, Acad Sci Ukrainian SSR

"Dok Ak Nauk SSSR" Vol LXXXIII, No 2, pp 257-260

New data supporting the essential similarity of the denaturation process of protein under all conditions were obtained by immunochem methods at the Inst of Biochem, Acad Sci Ukrainian SSR. In the denaturation of egg albumin by such agents as heat, alc, salicylate rhodanide, and copper ions, protein

214T27

prepns are obtained which by antigenic specificity contrast sharply with natural albumin, but are similar among themselves. A fundamental qual change in the macrostructure of the protein mols during its denaturation takes place, but the intermediate compn (apparently due to unstability of this stage) is not detected by ordinary methods. The ppt nature of the transformation attests to the fact that folding of polypeptide chains in the globule is produced by bonds that are mutually interdependent.

214T27

TSYPEROVICH, A. S.

"Investigation of the Denaturation and Stabilization of Globular Proteins." Dr Biol Sci, Laboratory of Enzymes, Inst of Biochemistry, Acad Sci USSR, Kiev, 1954, (KL, No 14, Apr 55)

SO: Sum. No. 704, 2 Nov 55 - Survey of Scientific and Technical Dissertations Defended at USSR Higher Educational Institutions (16).

TSYPEROVICH, A.S.

TSYPEROVICH, A.S.

[redacted]

Conference on the problem of proteins. Ukr.biokhim.zhur. 26 no.4: 467-474 '54. (MLRA 8:3)
(Proteins)

TSYPEROVICH, A.S.;LOSEVA, A.L.

Mechanism of protein denaturation. Report no.6: Denaturation of globular proteins without changing their viscosity and optical rotation. Ukr. biokhim. zhur. 27 no.4:494-502 '55. (MLRA 9:3)

1. Institut biokhimii Akademii nauk Ukrains'koi RSR, Kiiv.
(PROTEINS)

TSYPEROVICH, A.S.

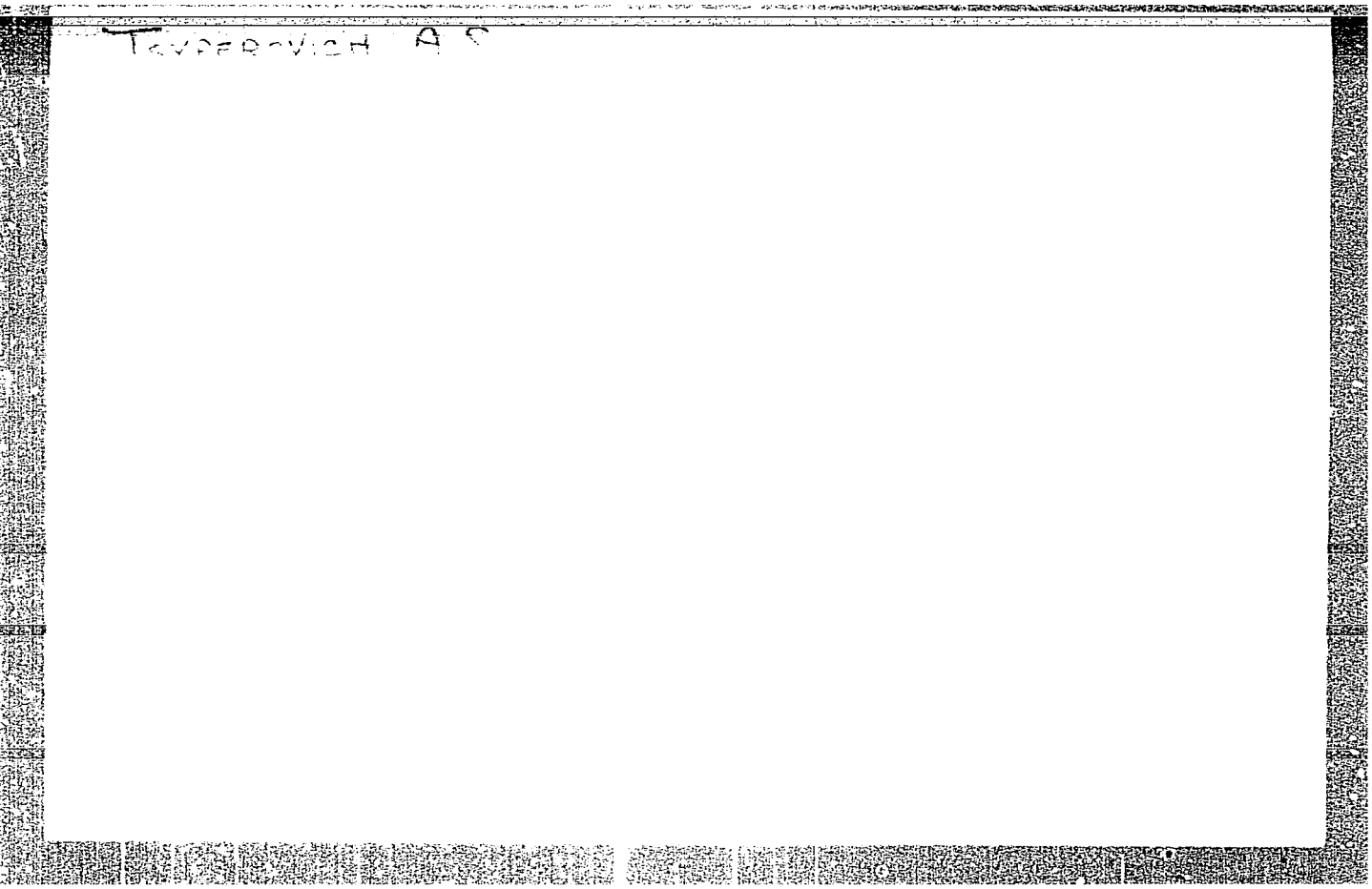
Mechanism of the denaturation of proteins; effect of formaldehyde and ether on the resistance to denaturation of globular proteins. Vop. med.khim. 2 no.3:169-174 My-Je '56. (MLRA 9:10)

1. Institut biokhimii AN USSR, Kiyev.
(PROTEINS,
denaturation, eff. of formaldehyde & ether on resist. (Rus))
(FORMALDEHYDE, effects,
on protein resist. to denaturation (Rus))
(ETHER, ETHYL, effects,
same)

TSYPEROVICH, A.S.; LOSEVA, A.L.

Mechanism of denaturation of proteins: new demonstration of the intermittent nature of denaturation of globular proteins. [with English summary in insert] Biokhimiia, 21 no.1:53-63 Ja-F '56. (MLRA 9:7)

1. Institut biokhimii Akademii nauk USSR, Kiyev.
(PROTEINS,
denaturation, intermittent nature of denaturation of globular proteins (Rus))



TSYPEROVICH, A.S.; LOSEVA, A.L.

Mechanism of the denaturation of proteins; properties of globular protein stabilized by the action of denaturating factor. Biokhimiia 21 no.5:546-556 S-O '56. (MLRA 9:12)

1. Institut biokhimii Akademii naik USSR, Kiyev.
(EGG WHITE,
ovalbumin, stabilization by denaturating factor (Rus))

TSYPEROVICH, A.S. (Kiyev)

Denaturation of globular proteins. Usp.khim.25 no.9:1173-1193 S '56. (MLRA 9:11)

(Proteins)

TSYPEROVICH, A.S.; LOSEVA, A.L.

Mechanism of protein denaturation. Report no.8: Materials on the characteristics of protein denaturation and the transformations connected with it. Ukr.biokhim.zhur. 28 no.3:265-277 '56. (MLRA 9:10)

1. Institut biokhimii Akademii nauk Ukrainskoy SSR, Kiyev.
(PROTEINS)

TSYPEROVICH, A.S.

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1.Vostochnyy uglekhimicheskiy institut (for TSynovnikov, Shemeryankin).
2.Ukrainskiy uglekhimicheskiy institut (for Shvarts, Bogoyavlenskiy).
(Coke)